FOAM-U 2019

iconCFD® Transonic A New Toolset for the Aerospace Industry



Prepared by: Vincent Rivola - Presenter Dr. Lucy Gagliardi – Transonic Product Leader



ICON PROFILE

Expert industry partner for more than 25yrs

- Simulation-driven product development
- 100+ CFD/CAE & Application specialists
- Largest OS CFD development team for industry
- Over 1000 customers of Group
- America Europe Asia
- Intel[®] Partner
- OS CFD market leader for automotive industry since 2004

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Solves the Navier-Stokes equations in a fully-implicit, density-based manner. The governing continuity, momentum and energy equations are treated as a fully coupled

system, in conservative form this is:

$$\frac{\partial \overrightarrow{W}}{\partial t} + \nabla \cdot \vec{F}_T = 0$$

• The equations are linearised in time, providing the following system:

$$\frac{\partial \vec{W}}{\partial t} + \nabla \cdot \left(\bar{\bar{J}}_T^o \delta W \right) = -\nabla \cdot \vec{F}_T^o$$

$$\begin{split} \overrightarrow{W} &= \begin{bmatrix} \rho \\ \rho \overrightarrow{U} \\ \rho E \end{bmatrix}, \quad \overrightarrow{F}_T = (\overrightarrow{F}_c - \overrightarrow{F}_v), \\ \overrightarrow{F}_c &= \begin{bmatrix} \rho \overrightarrow{U} \\ \rho \overrightarrow{U} \cdot \overrightarrow{U} + \overline{I}p \\ \rho \overrightarrow{U} \cdot H \end{bmatrix}, \\ \overrightarrow{F}_v &= \begin{bmatrix} 0 \\ \overline{\overline{\tau}}_{eff} \\ \overline{\overline{\tau}}_{eff} \cdot \overrightarrow{U} + \kappa \nabla T \end{bmatrix} \\ \overline{J}_T &= \frac{\partial \overrightarrow{F}_T}{\partial \overrightarrow{W}}, \quad \delta \overrightarrow{W} = \overrightarrow{W}^n - \overrightarrow{W}^o \end{split}$$

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iconCFD TRANSONIC INTRODUCTION - iconTransonicFoam

Solver developed in collaboration with ARA (UK).





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iconCFD TRANSONIC INTRODUCTION - iconTransonicFoam

• The system is solved for the **variable** $\delta \vec{W}$, with each component of the matrix comprising of the block Jacobian tensor and the source terms comprising of the vector fluxes.

$$\begin{bmatrix} \overline{\overline{I}} \\ \overline{\partial t} + \nabla \cdot \overline{J}_T^o \end{bmatrix} \delta \overrightarrow{W} = -\nabla \cdot \overrightarrow{F}_T^o$$

$$\downarrow \qquad \qquad \downarrow$$

$$\begin{bmatrix} \overline{\overline{A}} \end{bmatrix} \qquad \mathbf{x} \qquad = \qquad \overrightarrow{b}$$

- The system is discretised using a cell-centred finite volume approach.
- Convective fluxes use a 2nd order Roe formulation with Rebay-Van Leer flux limiter and modified Harten-Hyman entropy fix.
- Viscous fluxes use a 2nd order approximate central scheme with face gradient correction.
- Approximate formulations of the viscous and convective Jacobians are used.



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- RAE2822 2D Transonic aerofoil
- Experimental data from Cook et al. (AGARD-138)
- 2 cases considered:

Case*	<u>M</u>	<u>Re</u>	<u>T0 (K)</u>	<u>α(°)</u>
6	0.729	6,500,000	282	2.31
9	0.734	6,500,000	282	2.54

- Verification data from NASA (Wind3D), and EUROVAL project
- NPARC C-H structured mesh used for all cases
 - 23,552 cells
 - Average y+ ~ 1

*corrected for WT effects



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- Verification of Cp profile with data from NASA
 Wind3D code shows close agreement
- Suction peak and stagnation is predicted well compared to experimental results, although shock is slightly forward of experimental position.
- Force comparison is good with < 2 drag counts error to experiment.

	Lift				Drag	
Case	Pressure	Skin friction	Total	Pressure	Skin friction	Total
experiment	-	-	0.7340000	-	-	0.0127000
icon Transonic Foam	0.7113445	1.97E-05	0.7113642	0.0066840	0.0058293	0.0125133
Wind3D	0.7309260	3.63E-05	0.7309620	0.0062004	0.0059160	0.0121165



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- Classic validation test case for transonic flow
- Experimental data from Schmitt and Charpin (AGARD-AR-138) Test: 2308
- Test conditions:

М	Re	T0 (K)	<) α(°)	
0.8395	11,720,000	300	3.06	

- Verification data obtained from AIAA SciTech 2018 sessions: "RANS solutions for benchmark configurations"
- 3 codes: CFL3D, USM3D and FUN3D
- Geometry modified for a sharp TE (iconCFD case with original geometry)
- Ref. solutions run with Spalart-Allmaras neg model (iconCFD uses std SA)
- 4 consistent grid levels, L1-4

Mesh	nCells	
L1	69,206,016	
L2	8,650,752	
L3	1,081,344	
L4	135,168	
iconHexMesh	2,890,072	



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- *iconHexMesh* used to create mesh.
- aeroBlockMesh utility used to provide initial blocking and anisotropy framework around geometry.
- Hex-dominant mesh with full layer coverage and a y+ ~0.5
- Mesh size: ~2.89e6 cells







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- Comparing to CFL3D on all four mesh levels showed that iconTransonicFoam provides results comparable to the L1 mesh.
- Further verification of iconTransonicFoam will only be performed with the L1 mesh.



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- Comparison was also made to lift and drag coefficients for the L1 meshes
- Comparison is acceptable
- Slightly higher CI and Cd than the AIAA SciTech data correlates with Cp plots, particularly shock induced separation on outboard sections

	Mesh size	Lift	Drag		
Case	(nCells)	Total	Pressure	Skin friction	Total
iconTransonicFoam	2,890,072	0.2741	0.01393	0.00411	0.01803
CFL3D (L1 struct.)	69,206,016	0.2693	0.01165	0.00530	0.01696
USM3D (L1 tet.)	69,206,016	0.2706	0.01174	0.00531	0.01705
USM3D (L1 tet-prism)	69,206,016	0.2693	0.01168	0.00530	0.01698
FUN3D (L1 tet-prism)	69,206,016	0.2695	0.01167	0.00528	0.01695



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- 2nd AIAA Drag Prediction workshop: DLR F6 Wing/Body/Nacelle/Pylon configuration.
- Case 2: drag polar, fully turbulent.

Case	М	Re	ТО (К)	α (°)
2	0.7500	3,000,000	305.09	-3, -2, -1.5, -1, 0, 1, 1.5

- Verification data from the workshop on "medium" sized grid, ~8e6 cells.
- Comparison with a number of well-established codes, including: CFL3D, Cobalt, eLSA, ENSOLV, FUN3D, and TAU.
- Experimental results taken from data provided to workshop candidates.



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- iconHexMesh used to create mesh with comparable size to "medium" grids.
- aeroBlockMesh utility used to provide initial blocking and anisotropy framework around geometry.
- Hex-dominant mesh with near full layer coverage
- Mesh size ~10.43e6 cells
- Average y+ ~0.5
- Fully turbulent



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6-7-8-9-10-

- Force polar comparisons:
- FUN3D and Solver A also run fully turbulent









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iconCFD TRANSONIC VALIDATION – NASA TECH MEMO X778

 Model11 of the memo "Steady and fluctuating pressures at transonic speeds on hammerhead launch vehicles" is used as a validation case.





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• Mesh generation using iconHexMesh. Half domain contains 5M cells.





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• Mach 0.8 results and alpha 0deg, Mach number in the field, Cp at the wall:





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• Mach 0.8 results and alpha 0deg, Cp at the wall along the symmetryPlane:





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• Mach 1.17 results and alpha 0deg, Mach number in the field, Cp at the wall:





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• Mach 1.17 results and alpha 4deg, Mach number in the field, Cp at the wall:





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Mach 1.17 results and alpha 4deg, Cp at the wall along the symmetryPlane: 0.6--Cp extrados -Cp Intrados Cp exp 0.4 Cp exp 0.2n. -0.2-<mark>ද</mark> -0.4 -0.6--0.8--1--1.2--1.44 0.1 0,2 0.3 0.4 0.6 0.7 0.8 0.9 1.2 1.3 1.4 1.5 1.6 1.7 1.8 1.9 21 22 2.3 2.4 2.5 2.6 2.7 0.5 1.1 3 X(m)



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IDAJ CAE Solution Conference 2018

iconCFD TRANSONIC PROCESS

- The iconCFD Transonic module is not simply a solver
- Other tools within the module include:
 - aeroBlockMesh
 - Function objects on-the-fly post-processing modules
- Incorporated into the iconCFD workflow it can provide the user with a complete efficient, user-focused, automated process tailored to the aerospace industry.
 - Customisable App-based pre-processing
 - Geometry wrapping
 - Fully parallelised polyhedral meshing technology
 - Fully interactive generic post-processing viewer







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- Extend validation to transient data.
- DES simulation currently running







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THANK YOU – ANY QUESTION?





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